





TIM 2

Executive Summary

II. Broadband Passive AMCs

III. Reconfigurable AMCs

IV. Computational Tools Development

V. Schedule and Financial

VI. RECAP System Demonstration(s)

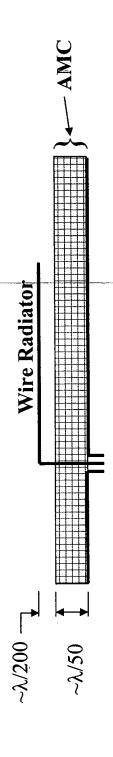








- ARCHES Basic Technical Approach
- 1. Create an electrically-thin Artificial Magnetic Conductor (AMC). a. High-impedance surface, $Z_s = E_{tan}/H_{tan}$, were $H_{tan} \sim 0$. b. Surface wave bandgap exists were $|Z_s| > \eta_o$.
- 2. Fabricate wire antenna elements in close proximity to the AMC. a. High gain, 4 to 6 dBil per element, occurs across the surface wave bandgap frequencies.



3. Electronically reconfigure both the element resonant frequency and the AMC resonant frequency for multi-band operation.







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Gain (dBiL) (measured at broadside)

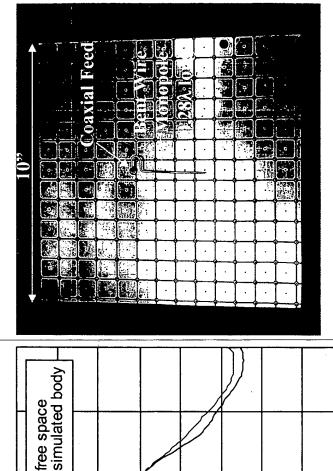
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Example of an AMC Antenna: Bent-Wire Monopole

free space



Bandwidth

Measured High Imp

gallon plastic bucket of tap water. Human torso simulated with a 5

1.65 1.6 1.55 Frequency (GHz) 4. 1.35 -10L 1.3

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entire high impedance bandwidth (bandgap)! High gain (~4 to 6 dBil) is available over the







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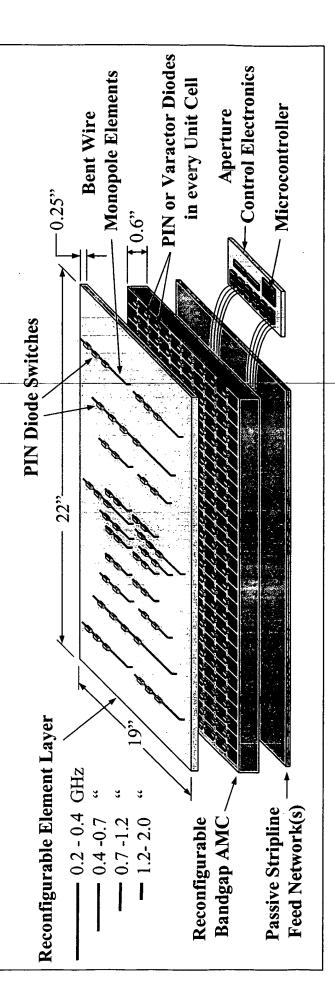




Proposed ARCHES 0.2-2.0 GHz Demonstration Array

ullet Very thin structure, ~ 1 inch thick (thinner for frequencies above $2~\mathrm{GHz})$ Features:

- Aperture area scales with frequency band relatively constant beamwidth
- Rapid electronic switching 10's of µsec



• UHF SATCOM Potential Applications:

· VHF LOS Comm.

· ULTRA-COMM · UHF LOS Comm.

• FOPEN JTIDS

JTRS

SUO

• ESM

· L-Band Data Links · SIGINT









ARCHES Program Goals

Task	Parameter	Goal
Passive AMC	Bandgap Bandwidth	Octave
	Thickness	$<\lambda_{\rm max}/50$
Reconfigurable AMC	Operational Bandgap	.2 - 2 GHz
	Thickness	<.75 inch
Reconfigurable Element	Instantaneous BW	15%
	Operational BW	Octave
	Element Gain	> 4 dBil
Array Demonstration	Operational Frequency	0.2 - 2 GHz
	Instantaneous BW	15%
	Array Size	19" x 22"
	Number of Elements	2 or 6
	Array Gain	12 dBil for the 6 element mode
		7 dBil for the 2 element mode
	Array Thickness	1 inch max.
	Fixed Beam	
	Computer Controlled	
Modeling and Simulation		1. New effective media models for AMCs
		2. Spectral domain analysis code for
		arrays of elements integrated into AMCs









ARCHES Task Description

Antennas in ReConfigurable High-impedance Electromagnetic Surfaces

- realize broadband and/or reconfigurable artificial magnetic conductors (AMCs) with embedded radiating elements. 1.0 Integrated Ground Plane (IGP) Technology Dev: Conduct research and technology development needed to
- 1.1 Passive Broadband AMC Dev.: Design, model, fabricate, and test hardware concepts for increasing the bandgap of AMCs. Both circuit and material approaches will be used. The goal is a 2:1 bandgap in the 0.2-2.0 GHz band.
- bandgap may be electronically reconfigured by controlling the reactive nature of the high-impedance surface 1.2 Reconfigurable Bandgap AMC Dev.: The basic goal is to realize a frequency tunable AMC, where the using arrays of solid state devices. The goal is to reconfigure the bandgap to cover 0.2-2.0 GHz.
- 1.3 Reconfigurable Radiating Element Dev.: Electronically switched radiators compatible with high-impedance surfaces will be modeled, built, and tested. The goal is to produce reconfigurable elements with a 10:1 operational bandwidth in the 0.2 to 2.0 GHz band.
- 1.4 Electronic Controller Dev.: Software and hardware will be created to control reconfigurable elements and AMCs.
- based on effective media models and MoM spectral domain algorithms. This task will be led by Rudy Diaz at ASU. 2.0 Computational Tool Dev.: Create electromagnetic modeling, simulation, and design tools for AMC structures
- 3.0 Antenna Array Demonstration: This task will integrate reconfigurable elements, a reconfigurable AIMC, and the electronic controller technology to create a 10:1 operational bandwidth array covering 0.2 - 2.0 GHz.
- 4.0 Program Management: TIM's, status reports, and technical reports.











What's New and Original with the ARCHES Program?

First 6 month's effort:

- · Techniques to increase the bandwidth of the Sievenpiper AMC concept
- Alternative AMC structures which differ from Sievenpiper's approach
- Techniques to electronically control or reconfigure the AMC bandgap(s)
- · New ideas for low cost printed antenna elements that can be integrated into AMC designs
- Concepts for effective media electromagnetic modeling of AMCs which may facilitate rapid design and analysis of AMC integrated antennas









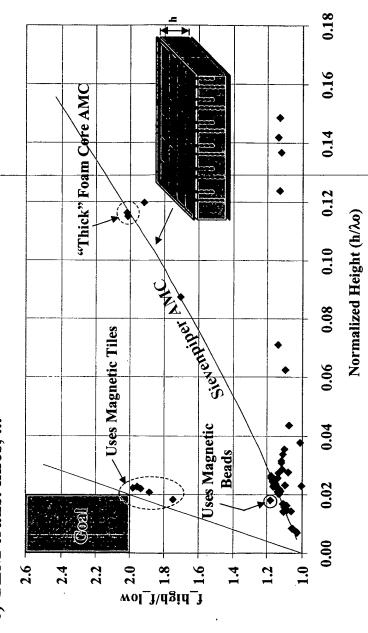
Progress on Broadband Passive AMCs

What has not worked: modifications using

- a) lumped inductors,
- b) septums
- c) TEM trans. lines, ...

What has worked: modifications using

- a) artificial magnetic materials
- b) magnetic beads



The use of Barium Cobalt hexaferrite tiles in a 400-800 MHz AMC design obtains a bandwidth performance very close to the goal.









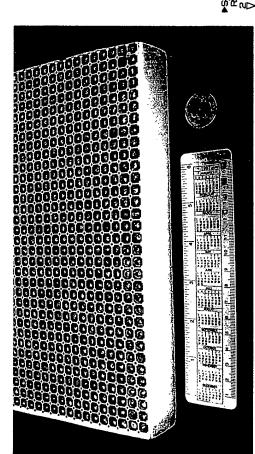


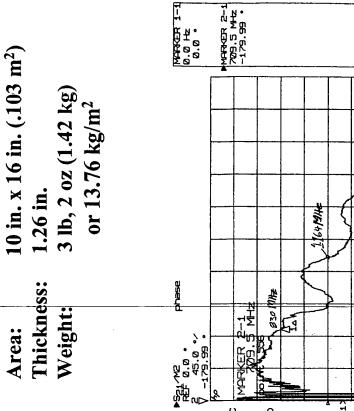
Non-Magnetic, Octave Bandwidth AMC

AMC_12-4, 800 MHz to 1600 MHz Goal

830 MHz to 1540 MHz.

Bandwidth:



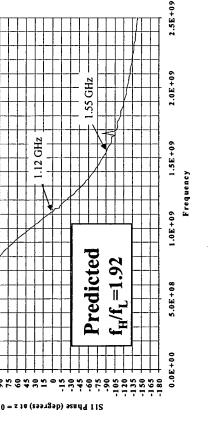


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BW = 741.25 MHz, $f_H/f_L = 1.92$, FBW = 66.2 %, $h/\lambda_o = 0.1139$, slope = 8.07

808.75 MHz --

1.12 GHz



Atlantic Aerospace Electronics Corporation



07 FEB 00 12:14:53

STOP 2. BORDBORDBORD GHZ

15.FP

START 0.500000000 GHz

Thinh = 186

Measured

 $f_{\rm H}/f_{\rm L}=1.86$





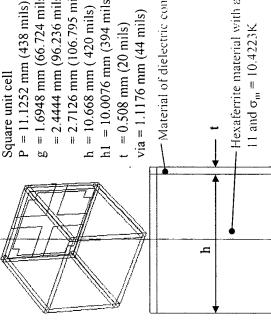


Magnetic, Octave Bandwidth AMC Design

AMC 34, 400 MHz to 800 MHz Goal



- · 400 MHz to 800 MHz
- $(\lambda/40 \text{ at } 600 \text{ MHz})$ • 0.475 inches thick
- · Unaligned Barium Cobalt hexaferrite tiles
- Weight = 9.8 lb/ft^2



= 2.7126 mm (106.795 mils) AMC 34-3 g = 1.6948 mm (66.724 mils) AMC_34 = 2.4444 mm (96.236 mils) AMC_34-2 h1 = 10.0076 mm (394 mils)h = 10.668 mm (420 mils)via = 1.1176 mm (44 mils)t = 0.508 mm (20 mils)

- Material of dielectric constant 3.38

- Hexaferrite material with $\varepsilon_r = 9$, $\mu_r =$ Via: One each located at the corners 11 and $\sigma_{\rm m} = 10.4223 \rm K$

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150 120 8 8 30

Incident Wave TEM Polarization:



1000

906

800

700

909

200

400

300

200

100

-150 -180

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SII Phase (degrees) at z = 0

Frequency (MHz)

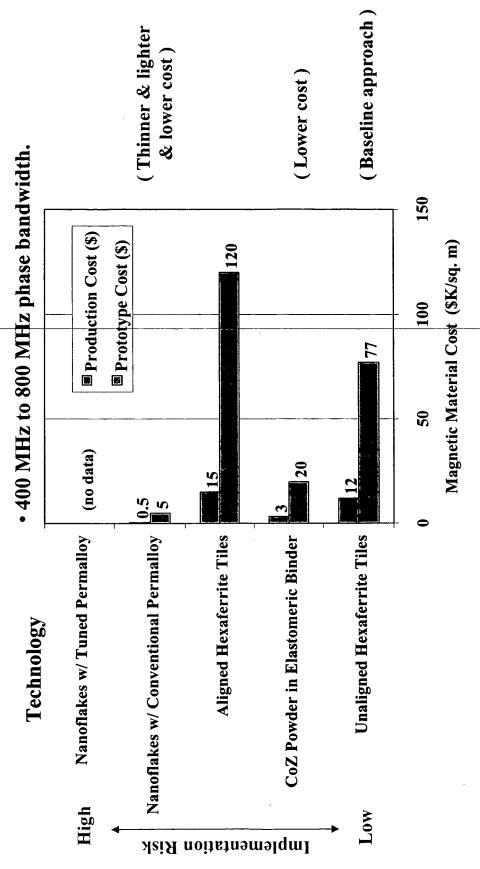






Estimated Cost of Artificial Magnetic Materials for an Octave Bandwidth AMC





Notes: 1. The AMC has a 400 MHz to 800 MHz phase bandwidth.

- 2. The cost of the printed FSS and backplane are estimated to be an additional \$2,000/(sq. m) in production.
 - 3. See Rodger Walser for a cost estimate of Nanoflakes with a Tuned Permalloy.

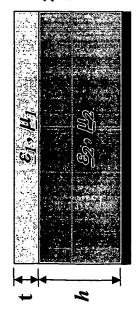








Effective Media Model of the Sievenpiper AMC



$$\begin{pmatrix} x & 0 & 0 \\ 0 & x & 0 \\ 0 & 0 & 0 \end{pmatrix} \circ \mathbf{3} = \mathbf{3}$$

Upper Layer*:
$$\varepsilon_{1xx} = \varepsilon_{1yy} = \frac{2b}{\pi t_1} \ln \left(\frac{2b}{\pi g} \right) \varepsilon_{avg}$$

$$\varepsilon_{1xx} = \varepsilon_{1yy} = \frac{\pi}{\pi t_1} \ln \left(\frac{\pi}{\pi g} \right) \varepsilon_{ax}$$

$$\varepsilon_{1zz} = 1$$

$$\mu_{1xx} = \mu_{1yy} = 1$$

$$\mu_{1xx} = \frac{\epsilon_{avg}}{\epsilon_{avg}}$$

$$1_{zz} = \frac{z_{zz}}{\epsilon_{1yy}}$$

where
$$\varepsilon_{avg} = \frac{1 + \varepsilon_D}{2}$$

$$\varepsilon_{2xx} = \varepsilon_{2yy} = \varepsilon_D \left(\frac{1+\alpha}{1-\alpha} \right)$$

$$\varepsilon_{2xx} = \varepsilon_{2yy} = \varepsilon_D \left(\frac{1 + \alpha}{1 - \alpha} \right) \qquad \mu_{2xx} = \mu_{2yy} = \frac{\varepsilon_D}{\varepsilon_{2xx}} \mu_D$$

$$\varepsilon_{2zz} = \varepsilon_D - \frac{1}{\omega^2 \varepsilon_0} \frac{\mu_D \mu_o A}{4\pi} \left[\ln \left(\frac{1}{\alpha} \right) + \alpha - 1 \right] \qquad \mu_{2zz} = (1 - \alpha)\mu_D$$

$$\varepsilon_D = \text{Relative permittivity of the background dielectric}$$

$$\mu_D = \text{Relative permeability of the background dielectric}$$

^{*}Assumes a single layer FSS with edge coupling









ARCHES Technical Status

- Completed 6 months of a 9 month passive AMC design effort. On schedule
- to create the 2:1 bandwidth AMC demo:
- Demonstrated a nonmagnetic, octave BW AMC with $h/\lambda_0 = .11$ (too thick)
- Magnetic tile, octave bandwidth AMC design is completed and now
- in fabrication with $h/\lambda_o = .02$
- Two additional artificial magnetic materials are being fabricated for AMCs:
- Barium Cobalt hexaferrite powder in an elastomeric binder
 - Permalloy nanoflakes in an elastomeric binder
- Completed a preliminary cost/weight/thickness study of artificial magnetic materials for AMCs
- Completed a 2 layer effective media model for the Sievenpiper AMC.
- Completed development of a transverse resonance model which predicts

TE and TM mode cutoff frequencies for the Sievenpiper AMC. (APS 2000 paper)











ARCHES Schedule, Milestones

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d Cost	
s, and	

Moni	Months ARO		Mar 2000								
Task	1-3	4-6	7-9	10-12	10-12 13-15 16-18	16-18		19-21 22-24	25-27	Cost (\$K)	Spent (\$K)
1 1 Passiva Broadband AMC				,	•						ļ
1.1 1 assive Divaudallu Alvie				2:1 Ba	2:1 Bandgap Demo	emo	····			331	235
1.2 Reconf. Bandgap AMC	**************************************	7723 40540				Recor	niig. AM	Reconfig. AMC Demo		552	0
1.3 Reconf. Elements		Solitor y					-	nfig. Ele	Reconfig. Elem. Demo	407	0
1.4 Electronic Controls		****** *								115	0
2. Computational Models							Final Code	ode 6 Elem	ode Element Arrav	610	47
3. Array Demo								.2-2 GI	.2-2 GHz Demo		0
4. Meetings & Tech Reports										234	99
Cost/Qtr (\$K)	305	166	321	535	483	371	145	177	36		
Cost/Year (\$K)		Yr.1	Yr 1 = 1,327		\mathbf{A}	Yr 2 = 1,176	,176		Yr 3 =36	=36	348 total



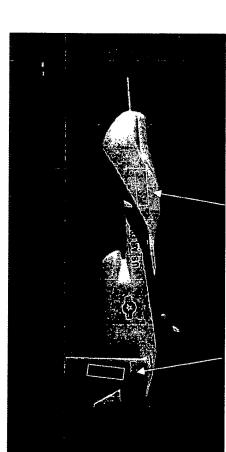








Thin, conformal, reconfigurable antennas for the dismounted-warfighter Potential ARCHES Program Payoff





					directional radiators	rtable applications	grated electronics
Benefits	1. "Paste-on" applications	2. Multi-function applications	3. Mobile and/or man-portable applications	4. Potential for low-cost fabrication	5a) Potential 3 dB gain improvement over bidirectional radiators	5b) Mitigation of body absortion for man-portable applications	5c) Mitigation of EMI/EMC effects with integrated electronics
Features	1. Electrically-thin aperture	2. Electronically reconfigurable in frequency	3. Lightweight	4. Printed antenna construction	5. Radiation is restricted to one hemisphere	due to the conducting backplane.	

